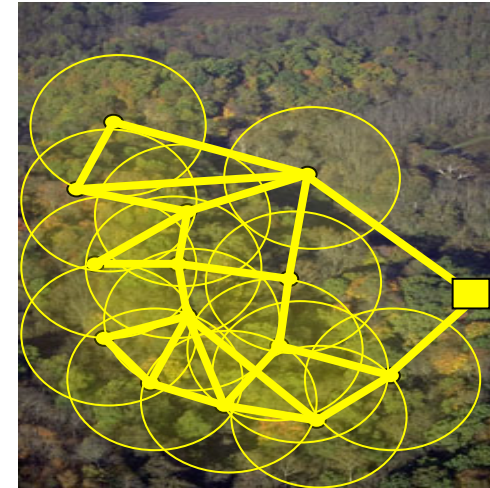


Analysis and Control of Flapping Flight: from Biological to Robotic Insects



Luca Schenato
Robotics and Intelligent Machines Laboratory
Department of EECS
University of California at Berkeley

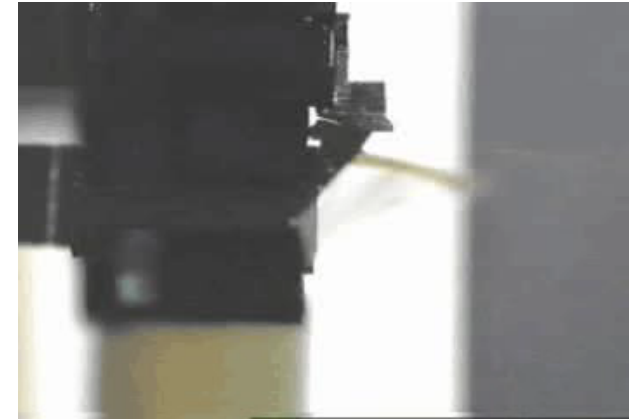
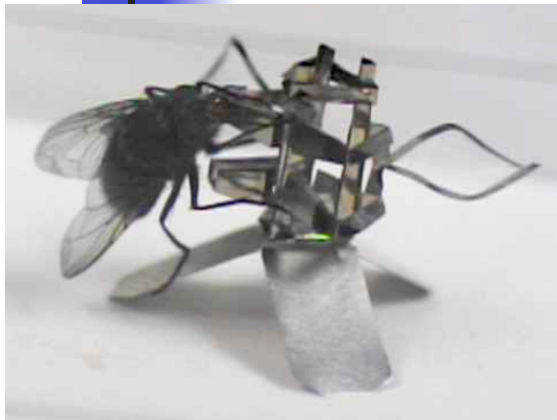


Biomimetic Flying Insects

- Overview and motivations
- True insect flight (Biomimetics)
- Averaging theory
- Flapping flight control

Micromechanical Flight Insect Project* (MFI)

*MURI-ONR



- **Objective:** 10-25mm (wingtip-to-wingtip), autonomous flapping flight, solar-cell powered, piezoelectric actuation, biomimetic sensors
- **Applications:** surveillance, search & rescue in hazardous and impenetrable environments
- **Advantages:** highly manoeuvrable, small, inexpensive
- **Interdisciplinary:** 4Dept (Bio,EE,ME,CS,Material S.), 6 profs., 10 students



Motivating Questions:

- **Biological perspective:**

- How do insects control flight ?
- Why are they so **maneuverable** ?

- **Engineering perspective:**

- How can we **replicate** insect flight performance on MFIs given the limited computational resources?
- How is flapping flight different from helicopter flight ?

- **Control Theoretic perspective:**

- What's really **novel** in flapping flight from a control point of view ?



Contribution:

- **Biological perspective:**

- Constructive evidence that flapping flight allows independent control of 5 degrees of freedom

- **Engineering perspective:**

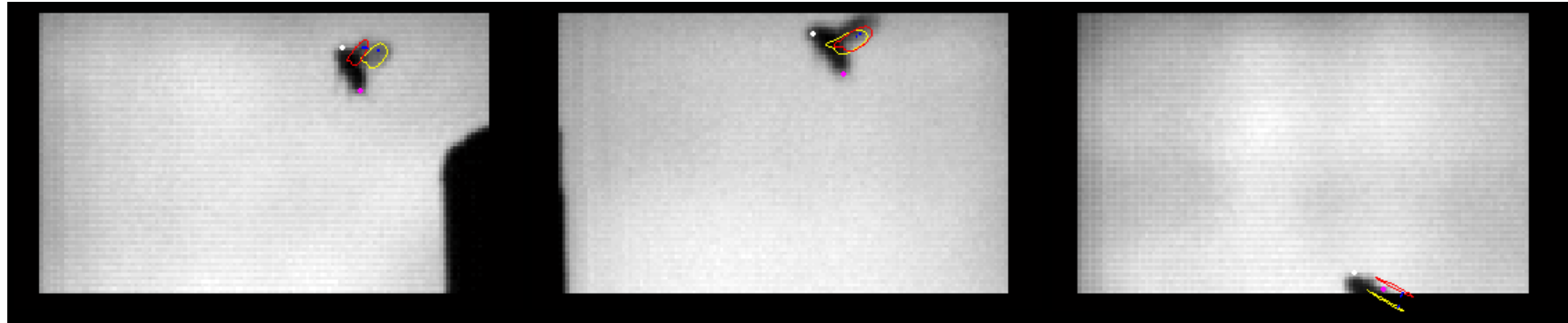
- Averaging theory and biomimetics simplify control design
- Periodic proportional feedback sufficient to stabilize several flight modes

- **Control Theoretic perspective:**

- Flapping flight as biological example of high-frequency control of an underactuated system

Previous work: biological perspective

Courtesy of S. Fry

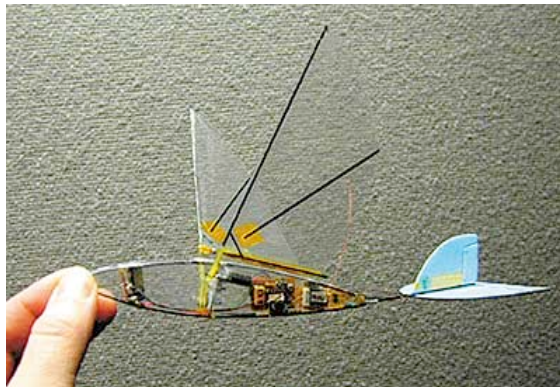


- Seminal work by C. Ellington and M. Dickinson for [insect aerodynamics](#) (80-90s)
- [Correlation](#) available between flight maneuvers and wing motions
- Partial evidence that insect can [control directly](#) 5 degrees of freedom out of the total 6



Previous work: Micro Aerial Vehicles (MAVs)

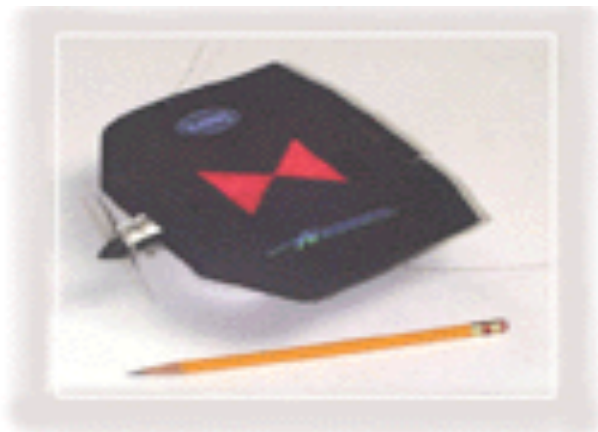
Microbat at Caltech



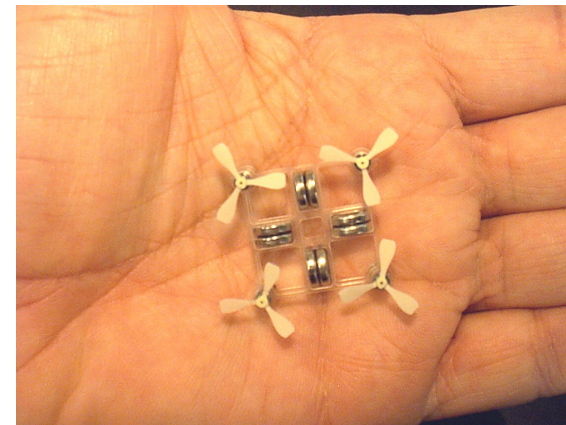
Entomopter at GeorgiaTech



Black Widow by Aerovinnment Inc.



Mesicopter at Stanford





Previous work: control theory

- **Fish locomotion:**

- [Mason, Morgansen, Vela, Murray, Burdick 99-03]
 - Underactuated systems
 - Averaging theory

- **Anguilliform locomotion (eels):**

- [McIsaacs 03, Ostrowski 98]
 - Symmetry
 - Averaging theory

- **Flapping flight**

- ... ?

**Periodic motion of appendages
is rectified into locomotion**

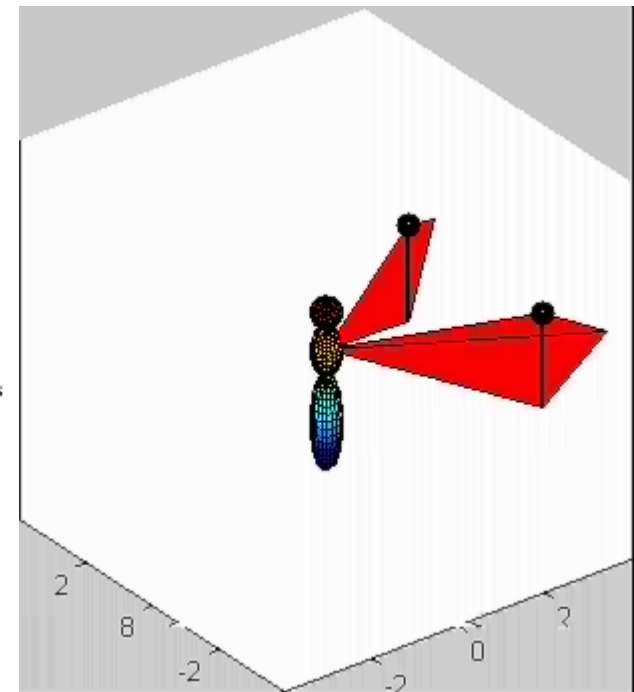
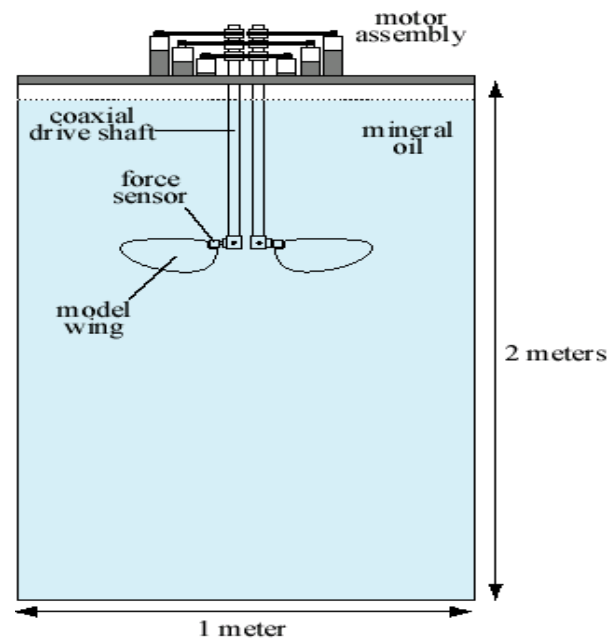
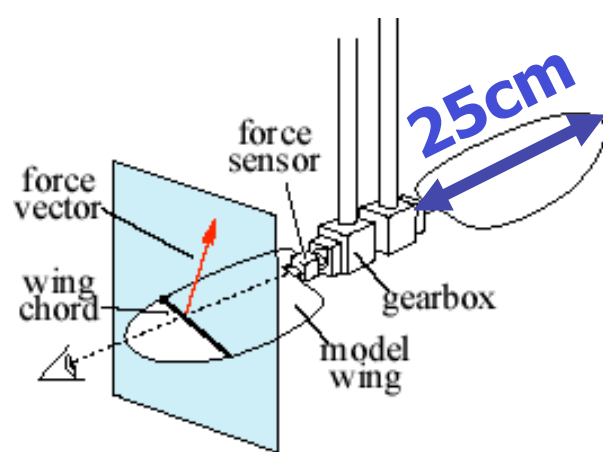


Biomimetic Flying Insects

- Overview and motivations
- True insect flight (Biomimetics)
- Averaging theory
- Flapping Flight Control

....The Bumblebee Flies Anyway

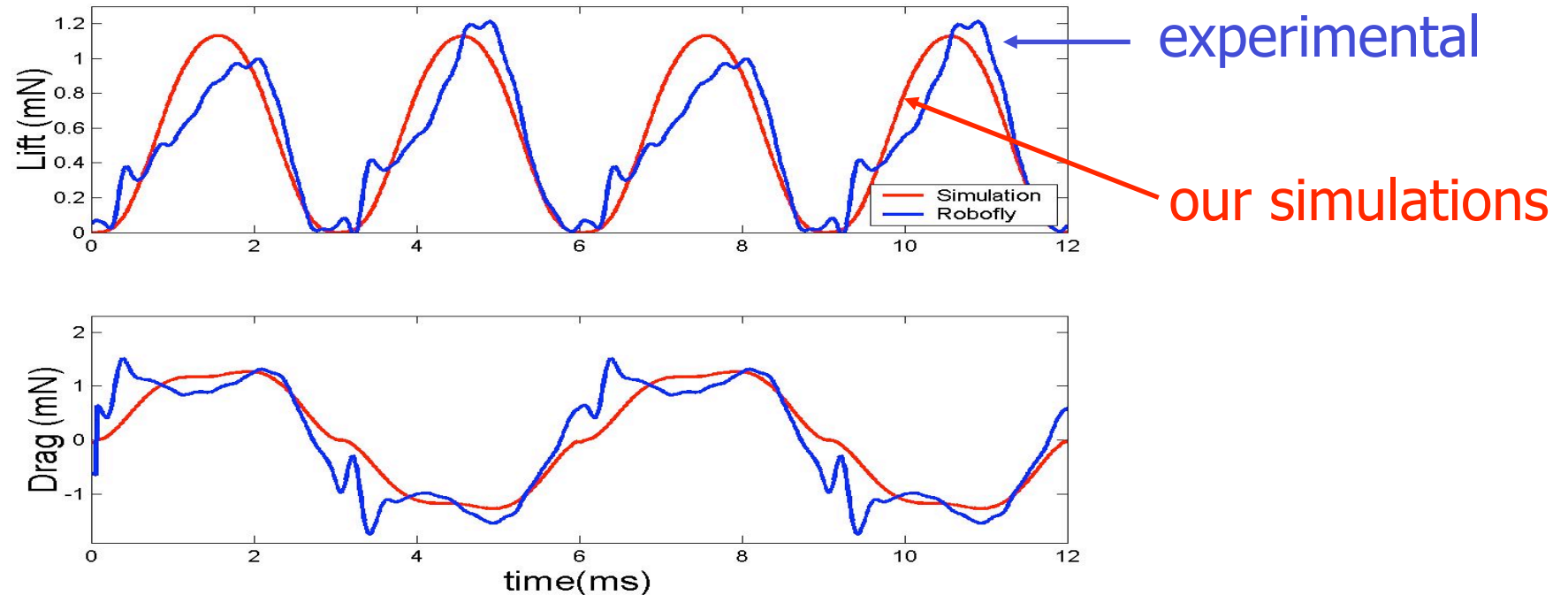
Unsteady state aerodynamics at low Reynolds Number $Re \approx 100-1000$



Courtesy of M.H. Dickinson and S. Sane

Aerodynamic Mechanisms:

Experimental data are courtesy of M.H. Dickinson and S. Sane



Delayed Stall

$$F_N = a V^2 \sin \alpha$$

Rotational lift

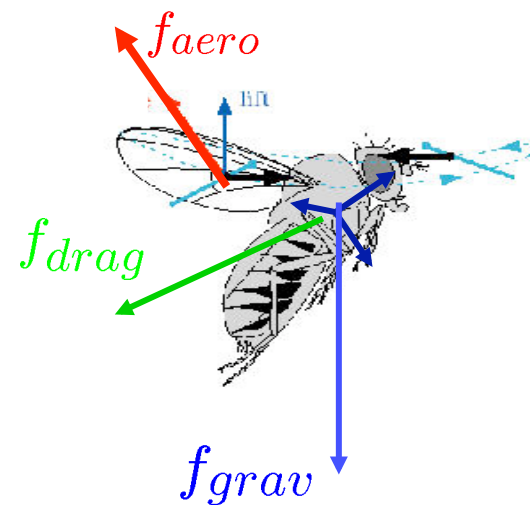
$$F_N = c V \dot{\alpha}$$

Wake Capture

Insect Body Dynamics

Rigid body motion equations

$$\begin{aligned}\dot{p} &= v^f \\ \dot{v}^f &= \frac{1}{m} R f_{aero}^b - g - \frac{c}{m} v^f \\ \dot{R} &= R \hat{\omega}^b \\ \dot{\omega}^b &= I_b^{-1} (\tau_{aero}^b - \omega^b \times I_b \omega^b)\end{aligned}$$



- $p \in \mathbb{R}^3$ – position
- $v^f \in \mathbb{R}^3$ – lin. velocity w.r.t fixed frame
- $R \in SO(3)$ – rotation matrix
- $\omega^b \in \mathbb{R}^3$ – ang. velocity w.r.t. body frame

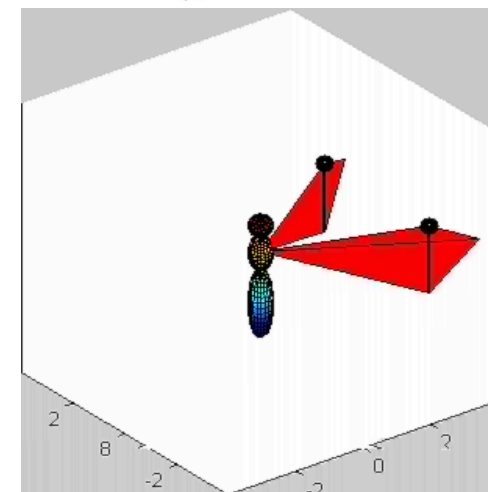
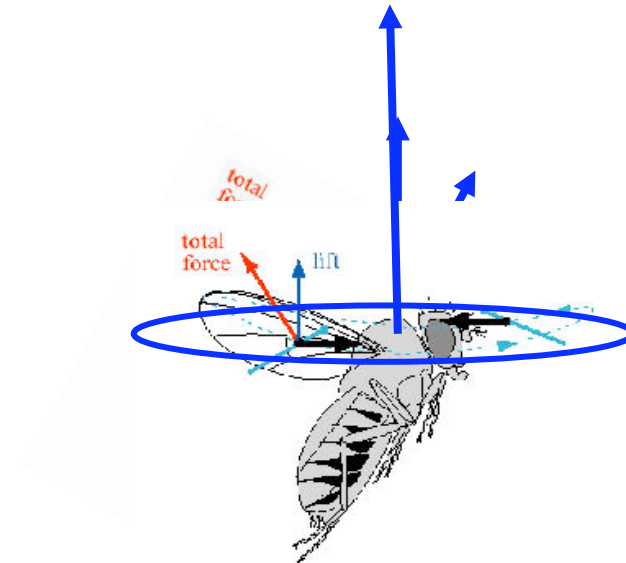
Insects and helicopters

■ Analogies:

- Control of position by changing the orientation
- Control of altitude by changing lift

■ Differences:

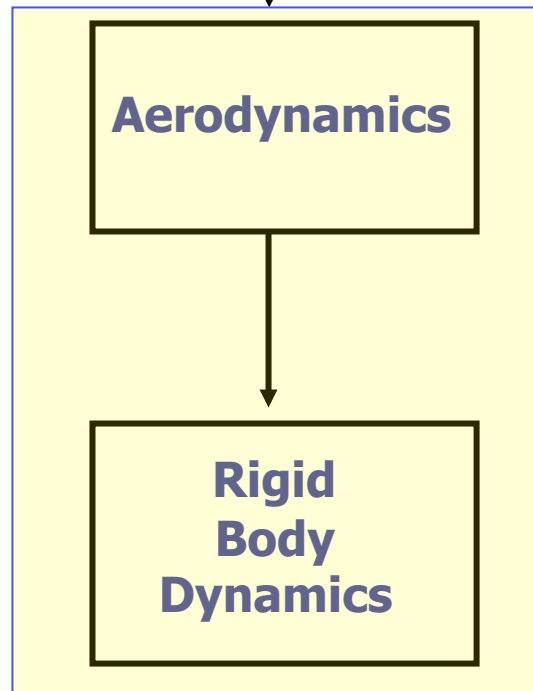
- Cannot control forces and torques directly since they are **coupled time-varying complex functions of wings position and velocity**



Dynamics of insect

Wing motion \downarrow $\begin{matrix} \phi_l(t), \phi_r(t) \\ \varphi_l(t), \varphi_l(t) \end{matrix}$

Input u



Insect motion \downarrow $\begin{matrix} p(t) \\ R(t) \end{matrix}$

Output x

$$\begin{aligned} \dot{p} &= v^f \\ \dot{v}^f &= \frac{1}{m} R \mathbf{f}_a(u) - g - \frac{c}{m} v^f \\ \dot{R} &= R \hat{\omega}^b \\ \dot{\omega}^b &= I_b^{-1} (\boldsymbol{\tau}_a(u) - \omega^b \times I_b \omega^b) \end{aligned}$$



Biomimetic Flying Insects

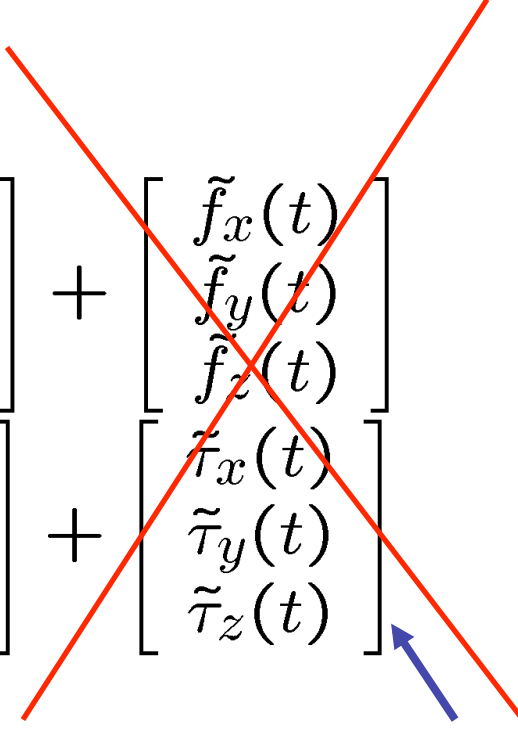
- Overview and motivations
- True insect flight (Biomimetics)
- *Averaging theory*
- Flapping Flight Control





Averaging Theory:

- If forces change very rapidly relative to body dynamics, only **mean** forces and torques are important

$$\begin{aligned} f_a^b(t) &= \begin{bmatrix} \bar{f}_x \\ \bar{f}_y \\ \bar{f}_z \end{bmatrix} + \begin{bmatrix} \tilde{f}_x(t) \\ \tilde{f}_y(t) \\ \tilde{f}_z(t) \end{bmatrix} \\ \tau_a^b(t) &= \begin{bmatrix} \bar{\tau}_x \\ \bar{\tau}_y \\ \bar{\tau}_z \end{bmatrix} + \begin{bmatrix} \tilde{\tau}_x(t) \\ \tilde{\tau}_y(t) \\ \tilde{\tau}_z(t) \end{bmatrix} \end{aligned}$$



 **Mean forces/torques**  **Zero-mean forces/torques**

Averaging Theory (Russian School '60s):

x: Periodic system

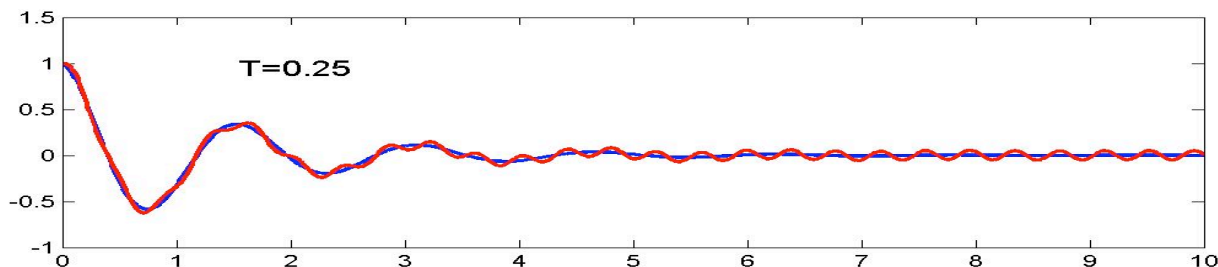
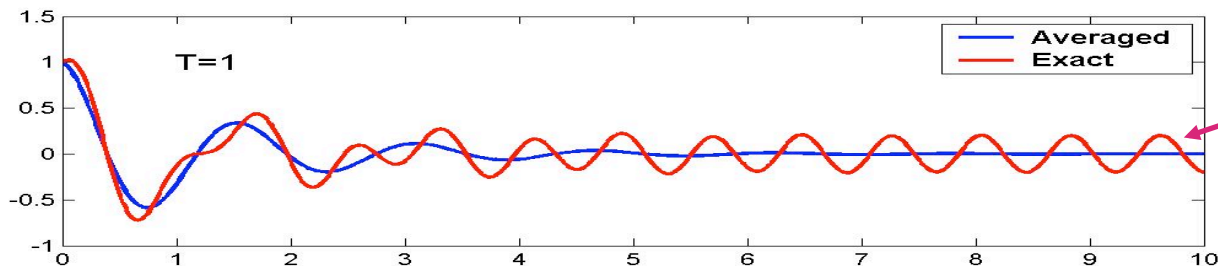
$$\dot{x} = f(x, t)$$

$$f(x, t) = f(x, t + T)$$

x_{av} : Averaged system

$$\dot{x}_{av} = \bar{f}_{av}(x_{av}) \leftarrow \text{Exponentially stable}$$

$$\bar{f}_{av}(x) \triangleq \frac{1}{T} \int_0^T f(x, \tau) d\tau$$





Averaging: systems with inputs

Original problem . Find a feedback law $g(x)$ such that the system

$$\begin{aligned}\dot{x} &= f(x, u) \\ u &= g(x)\end{aligned}$$

is asymptotically stable.



New Problem . Find periodic input $u = w(v, t)$ and a feedback law $h(x)$ such that the averaged system

$$\begin{aligned}\dot{x} &= \bar{f}_{av}(x, v) \\ \bar{f}_{av}(x, v) &= \frac{1}{T} \int_0^T f(x, w(v, \tau)) d\tau \\ v &= h(x)\end{aligned}$$

is asymptotically stable.

virtual inputs





Why ? 3 Issues

New Problem 1. Find periodic input $u = w(v, t)$ and a feedback law $h(x)$ such that the system

$$\begin{aligned} \dot{x} &= \bar{f}_{av}(x, v) \\ \bar{f}_{av}(x, v) &= \frac{1}{T} \int_0^T f(x, w(v, \tau)) d\tau \\ v &= h(x) \end{aligned} \quad (1)$$

is asymptotically stable.

Virtual inputs



- How do we choose the T-periodic function $w(v, t)$?
- How can we compute $\bar{f}_{av}(x, v) = \frac{1}{T} \int_0^T f(x, w(v, \tau)) d\tau$?
- How small should the period T be?

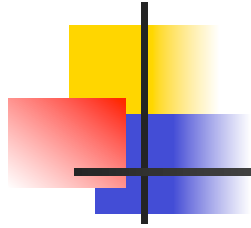


Advantages of high frequency: a motivating example

$$\begin{cases} \dot{x} = u^2 - 1 \\ \dot{y} = u \end{cases} \quad \begin{array}{l} 1 \text{ Input: } u \\ 2 \text{ Degrees of freedom: } (x,y) \\ \text{Want } (x,y) \rightarrow 0 \text{ for all initial conditions} \end{array}$$

- Origin $(x,y)=(0,0)$ is NOT an equilibrium point
- # degs of freedom $>$ # input available
(independently controlled)

Advantages of high frequency: a motivating example



Input is distributed differently

$$\begin{cases} \dot{x} = u^2 - 1 \\ \dot{y} = u \end{cases}$$

1 Input: u

2 Degrees of freedom: (x, y)

Want $(x, y) \rightarrow 0$ for all initial conditions

+

$$u = w(v, t) = v_1 + v_2 \sin \frac{t}{T}$$

↓

$$\begin{cases} \dot{\bar{x}} \approx v_2 - \sqrt{25}v_2^2 - 1^2 - 1 \\ \dot{\bar{y}} \approx v_1 \end{cases} \quad \begin{cases} v_2 = \sqrt{2} - \bar{x} \\ v_1 = -\bar{y} \end{cases}$$

Two linear independent virtual input: v_1, v_2 !!!!

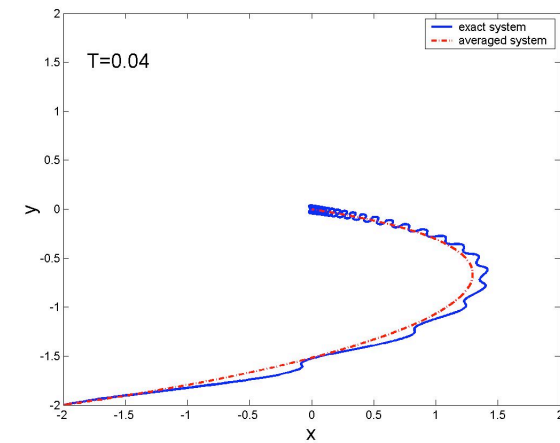
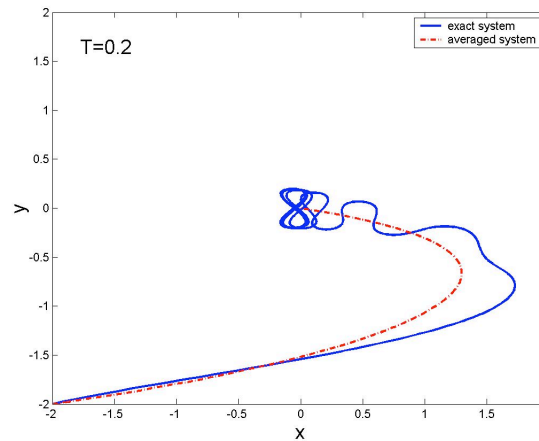
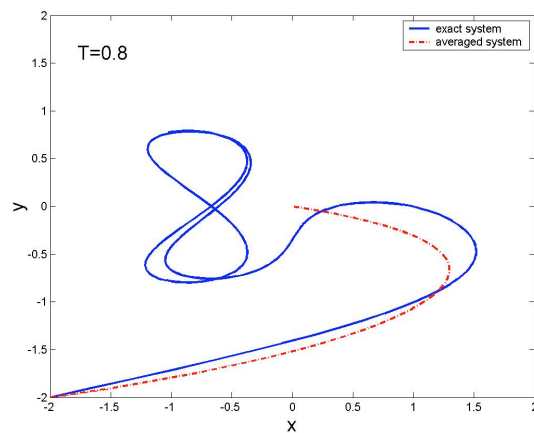
Advantages of high frequency: a motivating example

Closed loop system

$$\begin{cases} \dot{x} = u^2 - 1 \\ \dot{y} = u \\ u = -y + (\sqrt{2} - x) \sin \frac{t}{T} \end{cases}$$

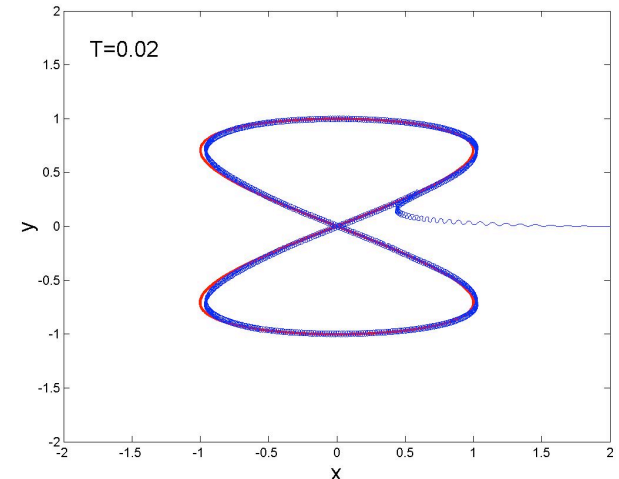
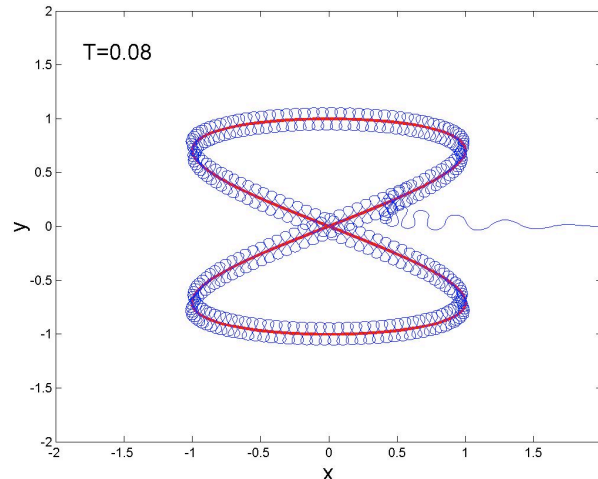
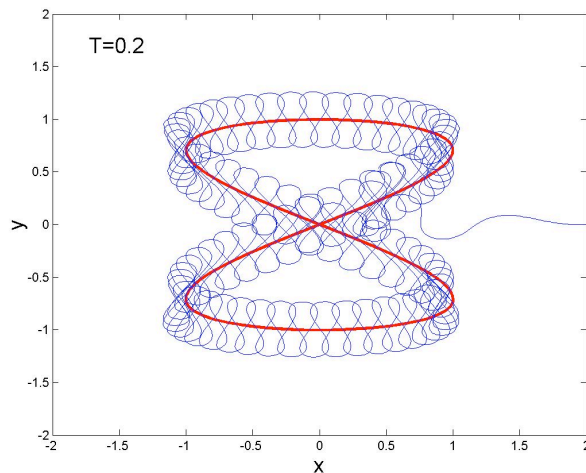
Averaged Closed loop system

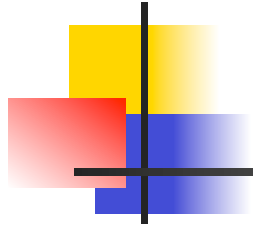
$$\begin{cases} \dot{\bar{x}} = \bar{y}^2 + 0.5(\sqrt{2} - \bar{x})^2 - 1 \\ \dot{\bar{y}} = -\bar{y} \end{cases}$$



Tracking "infeasible" trajectories

$$\begin{cases} \dot{x} = u^2 - 1 \\ \dot{y} = u \\ u = -(y - \sin(2t)) + (\sqrt{2} - (x - \sin(t))) \sin \frac{t}{T} \end{cases}$$





Advantages of averaging

1. Increases # of (virtual) inputs
2. Decouples inputs
3. Approximates infeasible trajectories



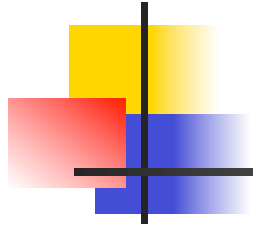
Back to the 3 Issues

- How do we choose the T-periodic function $w(v,t)$?
 - Geometric control [Bullo00] [Vela 03] [Martinez 03] ...
 - **BIOMIMETICS** : mimic insect wing trajectory
- How can we compute $\bar{f}(x, v) = \frac{1}{T} \int_0^T f(x, w(v, t)) dt$?
 - For insect flight this boils down to computing **mean forces and torques** over a wingbeat period:
- How small must the period T of the periodic input be?
 - **Practically** in all insect species wingbeat period T is small enough w.r.t insect dynamics



Biomimetic Flying Insects

- Overview and motivations
- True insect flight (Biomimetics)
- Averaging theory
- Flapping Flight Control



The 3 Issues

- How do we choose the T-periodic function $u=w(v,t)$?
- How can we compute $\bar{f}(x, v) = \frac{1}{T} \int_0^T f(x, w(v, t)) dt$?
- How small must the period T of the periodic input be?

Flight Control mechanisms in real insects



- Kinematic parameters of wing motion have been correlated to observed maneuvers [[G. Taylor, Biol. Rev. 99](#)]
 - **Stroke amplitude:**
 - Symmetric change → climb/dive
 - Asymmetric change → roll rotation
 - **Stroke offset:**
 - Symmetric change → pitch rotation
 - **Timing of rotation**
 - Asymmetric → yaw/roll rotation
 - Symmetric → pitch rotation
 - **Angle of attack**
 - Asymmetric → forward thrust



Parameterization of wing motion

$$u = w(v, t) = g_0(t) + G(t)v$$

Stroke angle

Stroke amplitude

Offset of stroke angle

Rotation angle

Timing of rotation

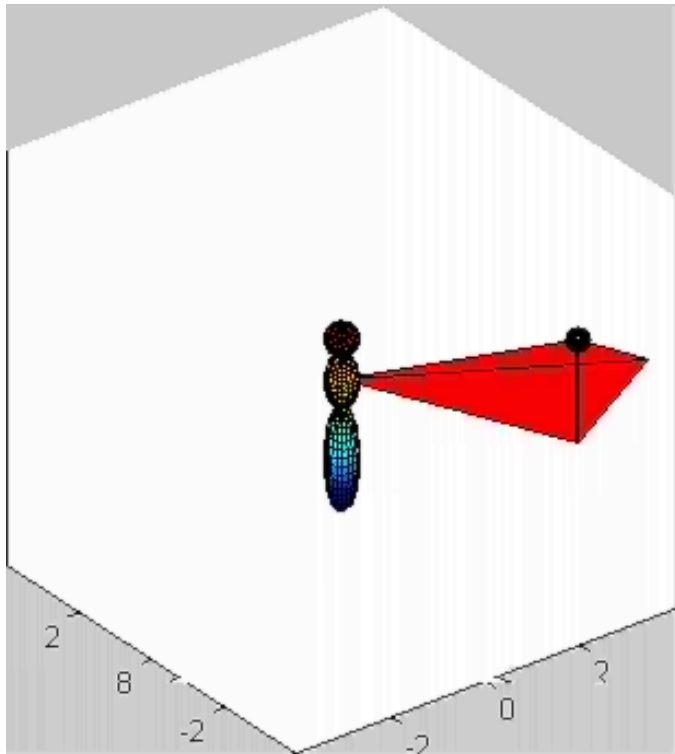
$$\begin{aligned} u_{1,i} &= \frac{\pi}{3} \cos(\omega t) + v_1 \frac{\pi}{6} \cos(\omega t) + \frac{\pi}{15} v_2 \\ u_{2,i} &= \frac{\pi}{4} \sin(\omega t) + v_3 \frac{\pi}{4} \sin^3(2\omega t) \end{aligned}$$

$(i \in \{l, r\})$

Parameterization of wing motion

$$u_{1,i} = \frac{\pi}{3} \cos(\omega t) + v_1 \frac{\pi}{6} \cos(\omega t) + \frac{\pi}{15} v_2$$

$$u_{2,i} = \frac{\pi}{4} \sin(\omega t) + v_3 \frac{\pi}{4} \sin^3(2\omega t)$$



-60 **0** **60**
 $v_1 = 1$ $v_1 = 0$ $v_1 = -1$

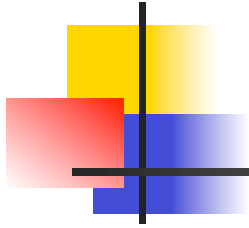


-60 **0** **60**
 $v_3 = 1$ $v_3 = 0$ $v_3 = -1$



Back to the 3 issues

- How do we choose the T-periodic function $w(v,t)$?
- How can we compute $\bar{f}(x, v) = \frac{1}{T} \int_0^T f(x, w(v, t)) dt$?
- How small must the period T of the periodic input be?

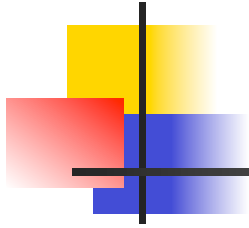


Mean forces/torques map

Independent control of 5 degrees of freedom

$$|v_i| \leq 1 \begin{bmatrix} \bar{f}_x \\ \bar{f}_y \\ \bar{f}_z \end{bmatrix} \approx \begin{bmatrix} 0 \\ 0 \\ mg \end{bmatrix} + 0.2mg \begin{bmatrix} v_3^l + v_3^r \\ 0 \\ v_1^l + v_1^r \end{bmatrix}$$
$$\begin{bmatrix} \bar{\tau}_x \\ \bar{\tau}_y \\ \bar{\tau}_z \end{bmatrix} \approx 0.2mgL \begin{bmatrix} v_1^l - v_1^r \\ v_2^l + v_2^r \\ v_3^l - v_3^r \end{bmatrix}$$

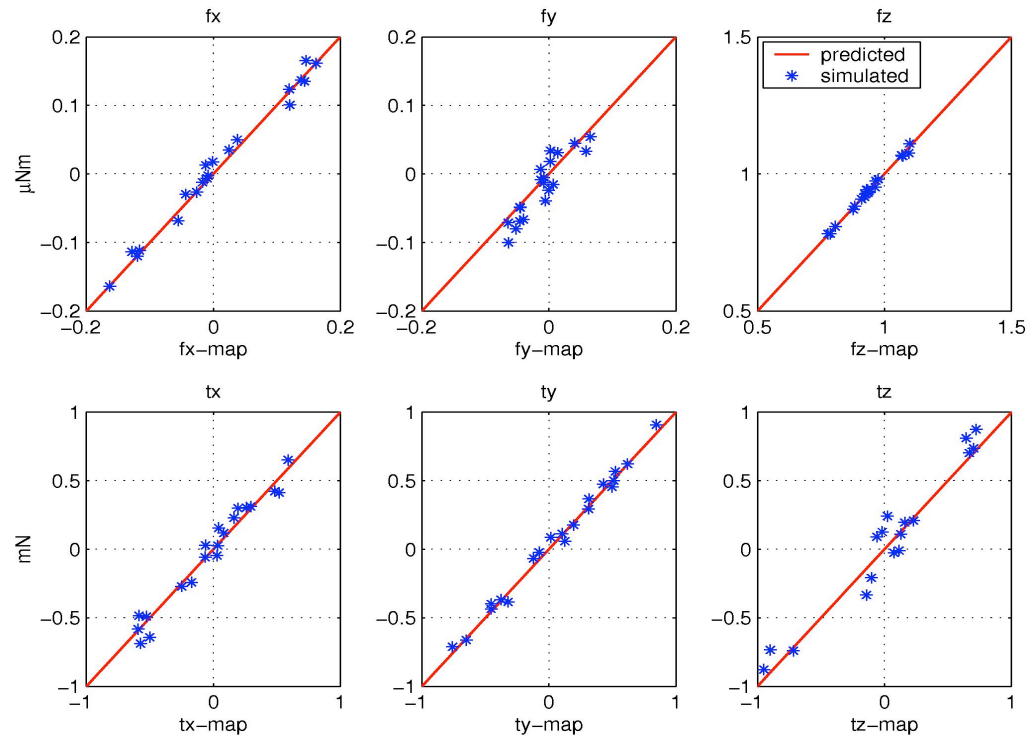
Wing length



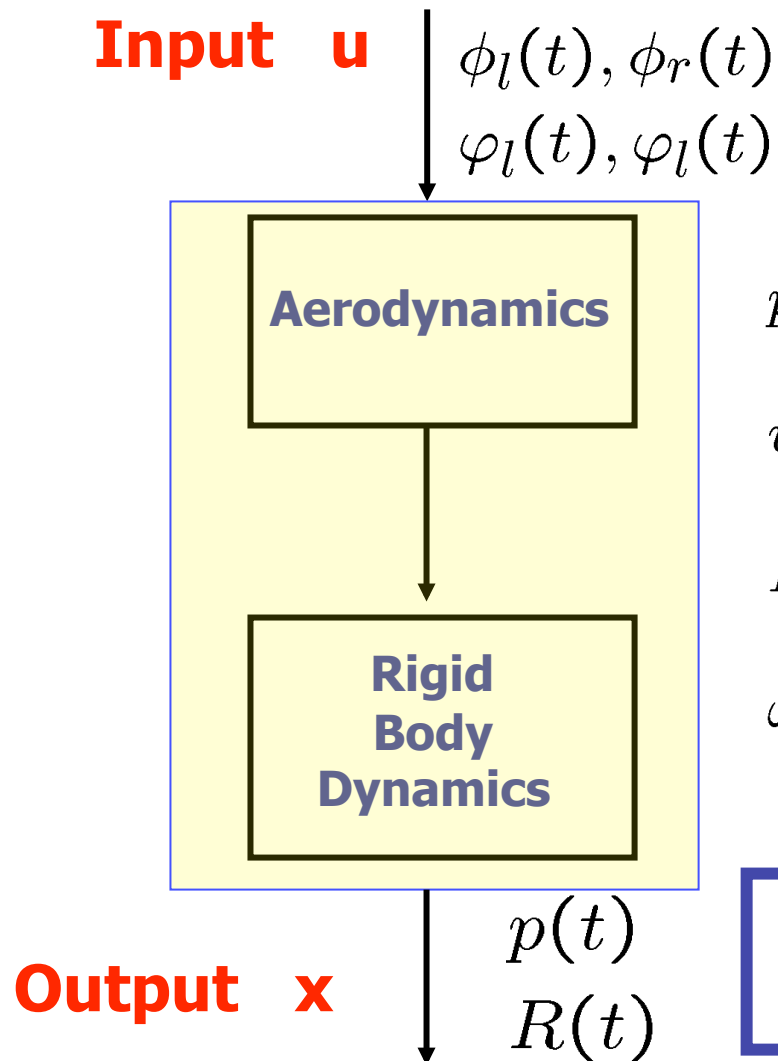
Mean forces/torques map

$$\begin{bmatrix} \bar{f}_x \\ \bar{f}_y \\ \bar{f}_z \end{bmatrix} \approx \begin{bmatrix} 0 \\ 0 \\ mg \end{bmatrix} + 0.2mg \begin{bmatrix} v_3^l + v_3^r \\ 0 \\ v_1^l + v_1^r \end{bmatrix}$$

$$\begin{bmatrix} \bar{\tau}_x \\ \bar{\tau}_y \\ \bar{\tau}_z \end{bmatrix} \approx 0.2mgL \begin{bmatrix} v_1^l - v_1^r \\ v_2^l + v_2^r \\ v_3^l - v_3^r \end{bmatrix}$$



Dynamics of insect revised

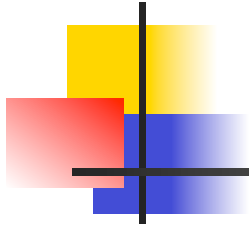


Before averaging

$$\begin{aligned} \dot{p}_m &= v^f \\ \dot{v}_m^f &= \frac{1}{m} R \begin{bmatrix} \tilde{v}_1 \\ 0 \\ \tilde{v}_2 \end{bmatrix} - g - \frac{c}{m} v^f \quad f \\ \dot{R}_m &= R \hat{\omega}^b \\ \dot{\omega}_m^b &= I_b^{-1} \left(\begin{bmatrix} \tilde{v}_3 \\ \tilde{v}_4 \\ \tilde{v}_5 \end{bmatrix} - \omega^b \times I_b \omega^b \right) \end{aligned}$$

$$v = Kx$$

- Hovering
- Cruising
- Steering



Proportional periodic feedback

BIOMIMETICS

Wings trajectory

$$u = g_0(t) + G(t)v$$

Kinematic parameters

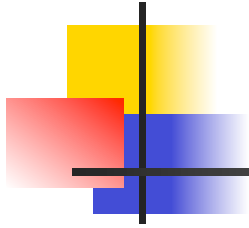
Averaging LQG, H_∞, \dots

Insect position

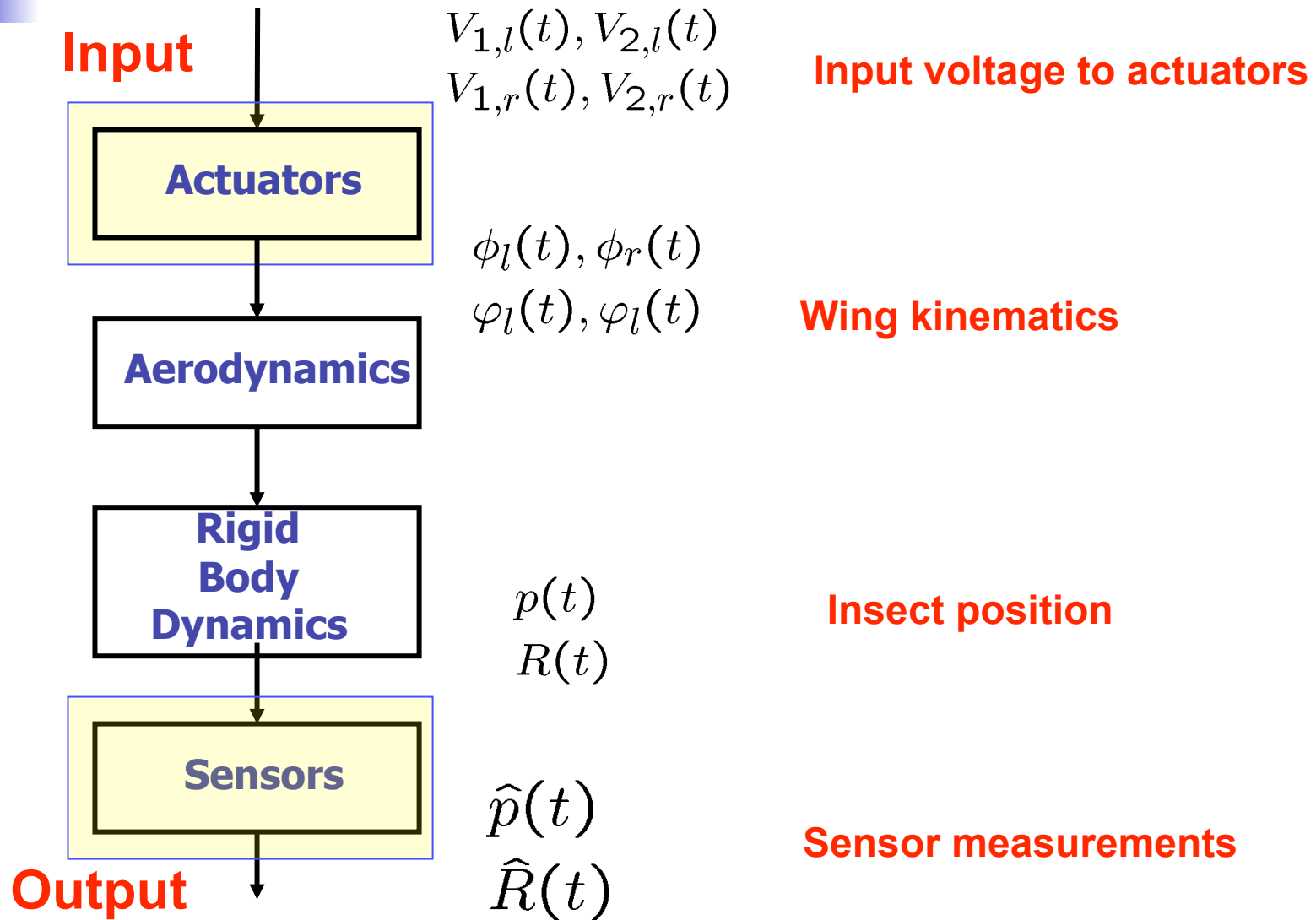
$$v = Kx$$

$$u = g_0(t) + \tilde{G}(t)x$$

Periodic proportional feedback



Insect Dynamics: realistic model





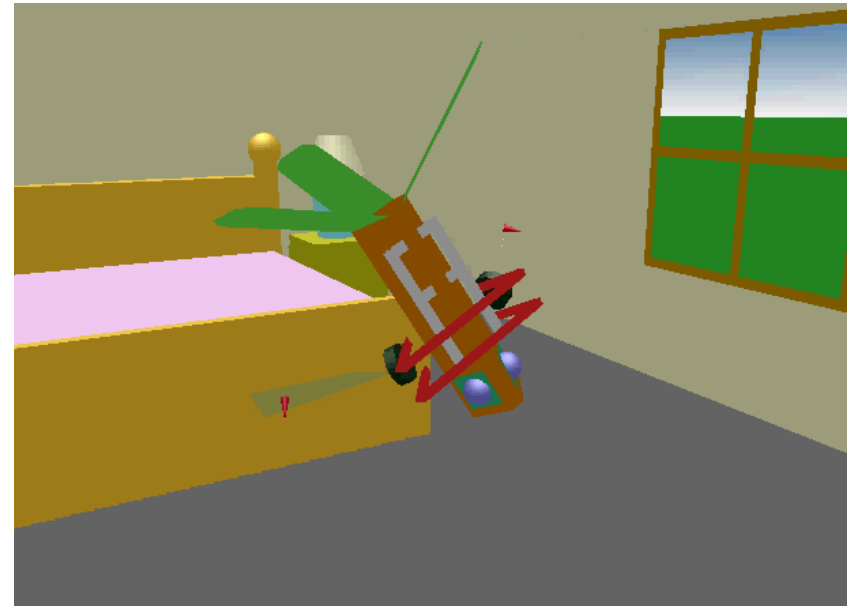
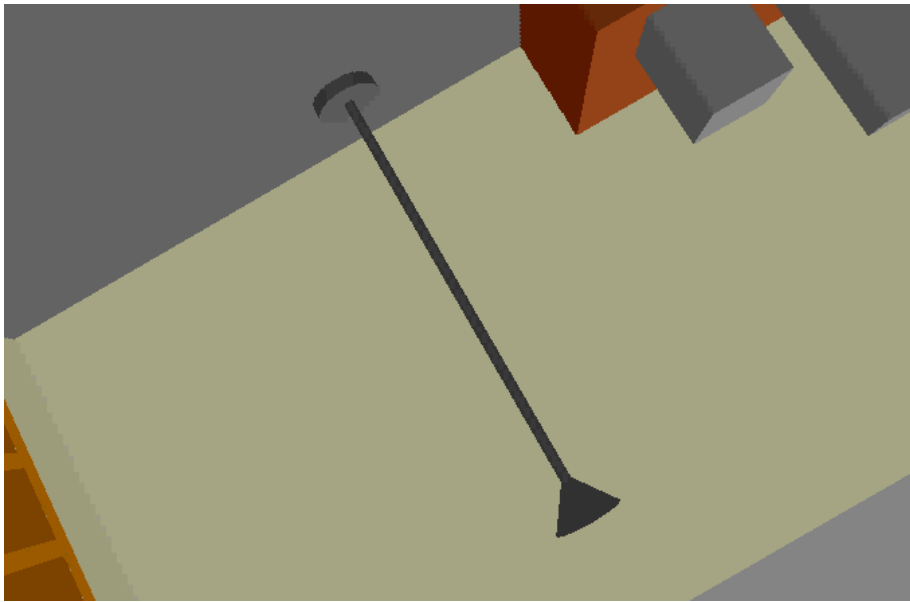
Proportional periodic feedback

Output from sensors

Input voltages to actuators

$$\begin{bmatrix} V_{1,l}(t) \\ V_{2,l}(t) \\ V_{1,r}(t) \\ V_{2,r}(t) \end{bmatrix} = h(t) + \tilde{H}(t) \begin{bmatrix} y_c \\ y_1^o \\ y_2^o \\ y_x^h \\ y_y^h \\ y_z^h \end{bmatrix}$$

Simulations w/ sensors and actuators: Recovering





Summarizing ...

- **Biological perspective:**

- Flapping flight allows independent control of 5 degrees of freedom

- **Engineering perspective:**

- Averaging theory and biomimetics simplify control design
- Periodic proportional feedback sufficient to stabilize several flight modes

- **Control Theoretic perspective:**

- Flapping flight as biological example of high-frequency control of an underactuated system

What's next ?

Bird flocks



Insect swarms



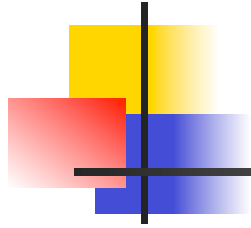
Fish schools



■ **Fundamental questions:**

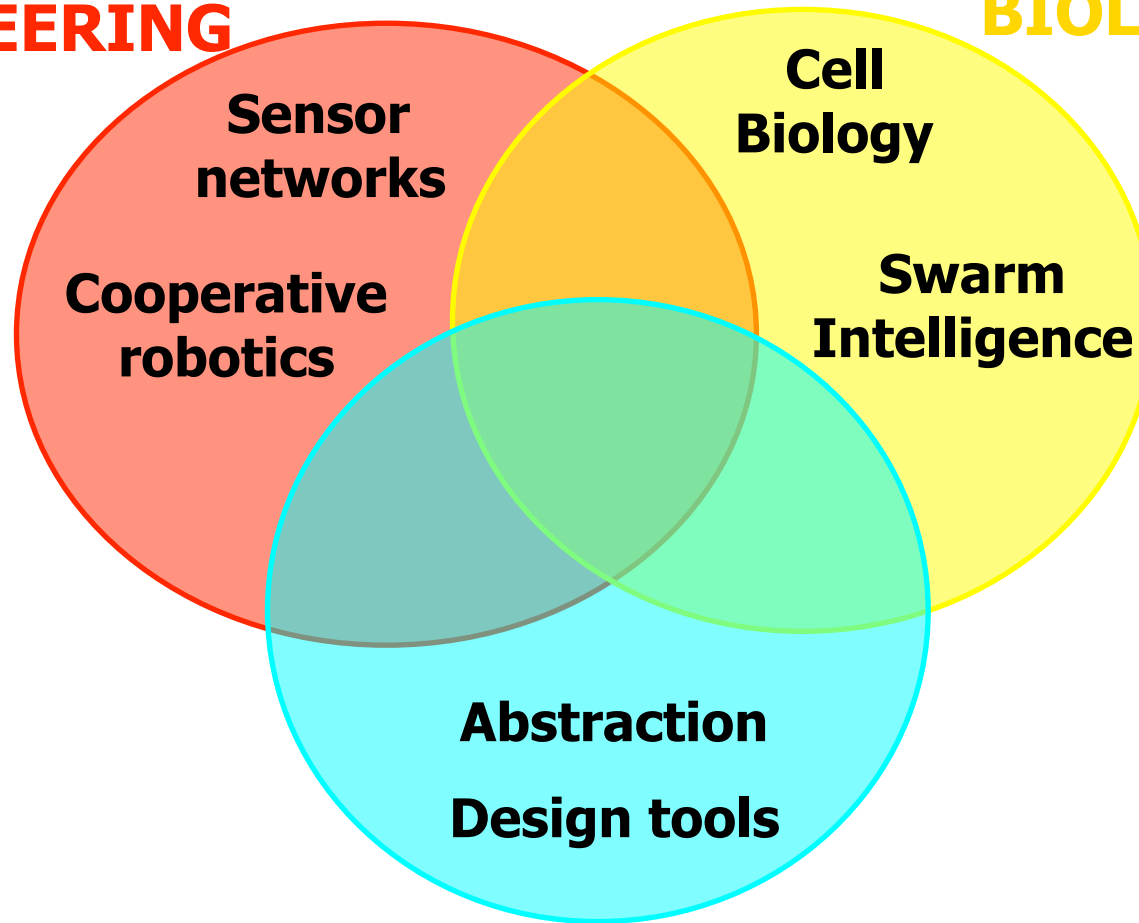
- How **local feedback** and **communication** give rise to **global behavior** ?
- How is **information extracted** and **propagated** over the network ?
- How **spatial** and **temporal** correlation is exploited ?

Research agenda: networks of systems



ENGINEERING

BIOLOGY



SYSTEMS THEORY



Publications:

- **Analysis and Control of flapping flight: from biological to robotic insect**, Ph.D. dissertation, 2003
- **Attitude Control for a Micromechanical Flying Insect via Sensor Output Feedback** with **W.C Wu, S. Sastry**, IEEE Trans Rob.&Aut., Feb 2004
- **Flapping flight for biomimetic robotic insects: Part I - System modeling** with **W.C Wu, X. Deng S. Sastry**, submitted to IEEE Trans. Robotics
- **Flapping flight for biomimetic robotic insects: Part II – Flight Control Design** with **X. Deng, S. Sastry**, submitted to IEEE Trans. Robotics